

NORTH

**Map Sources:**

USGS 7.5' Topographic Maps 2015, Laytonville,  
Mendocino County, California, Scale 1:24000



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**GEOTECHNICAL INVESTIGATION**  
**LAYTONVILLE DOS RIOS ROAD**  
**(CR 322) FAILURE AT MP 3.34**

LAYTONVILLE, MENDOCINO CO., CA

**Figure 1**  
Vicinity Map

Prj. No: 16-337.10

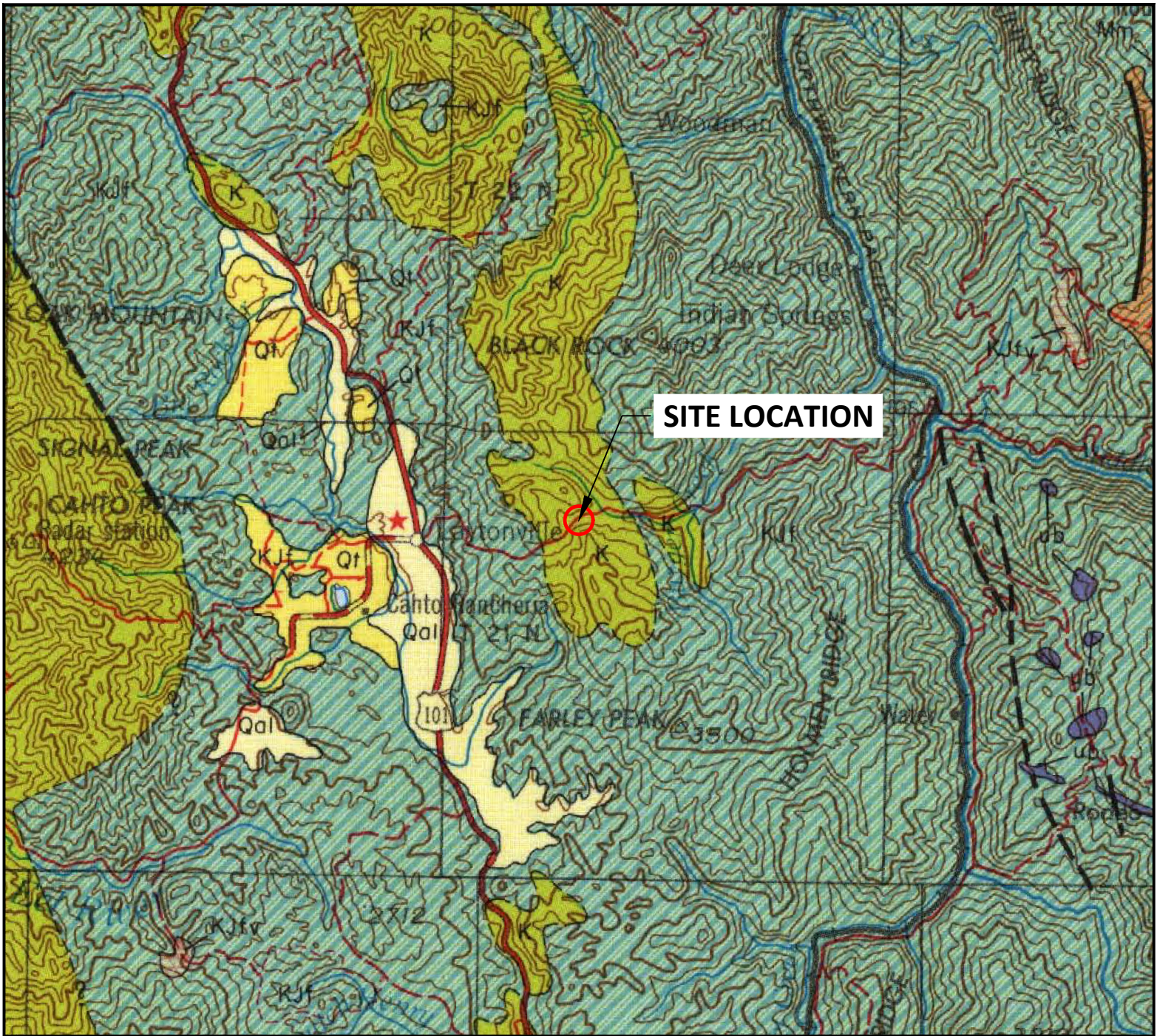
Scale: 1" = 2,500'

Date: 12/15/2017









## LEGEND

### Geologic Formations



**Alluvium (Recent)** - alluvial materials (sand, silt, clay); valley fill.



**Undivided Marine Sedimentary Rocks (Cretaceous)** - sandstone, shale, and conglomerate.



**Franciscan Formation (Jurassic-Cretaceous)** - sandstone, shale, chert, and conglomerate, with locally small areas of greenstone, limestone, basalt, schist, and related metamorphic rocks.



**CONTACT**

(Dashed where approximately located, gradational or inferred)



**FAULT**

(Dashed where approximately located)



**NORTH**

#### Map Source:

Jennings, C.W. and Strand, R.G., 1960, *Geologic Map of California, Ukiah Sheet, California Division of Mines and Geology*, Scale 1:250,000



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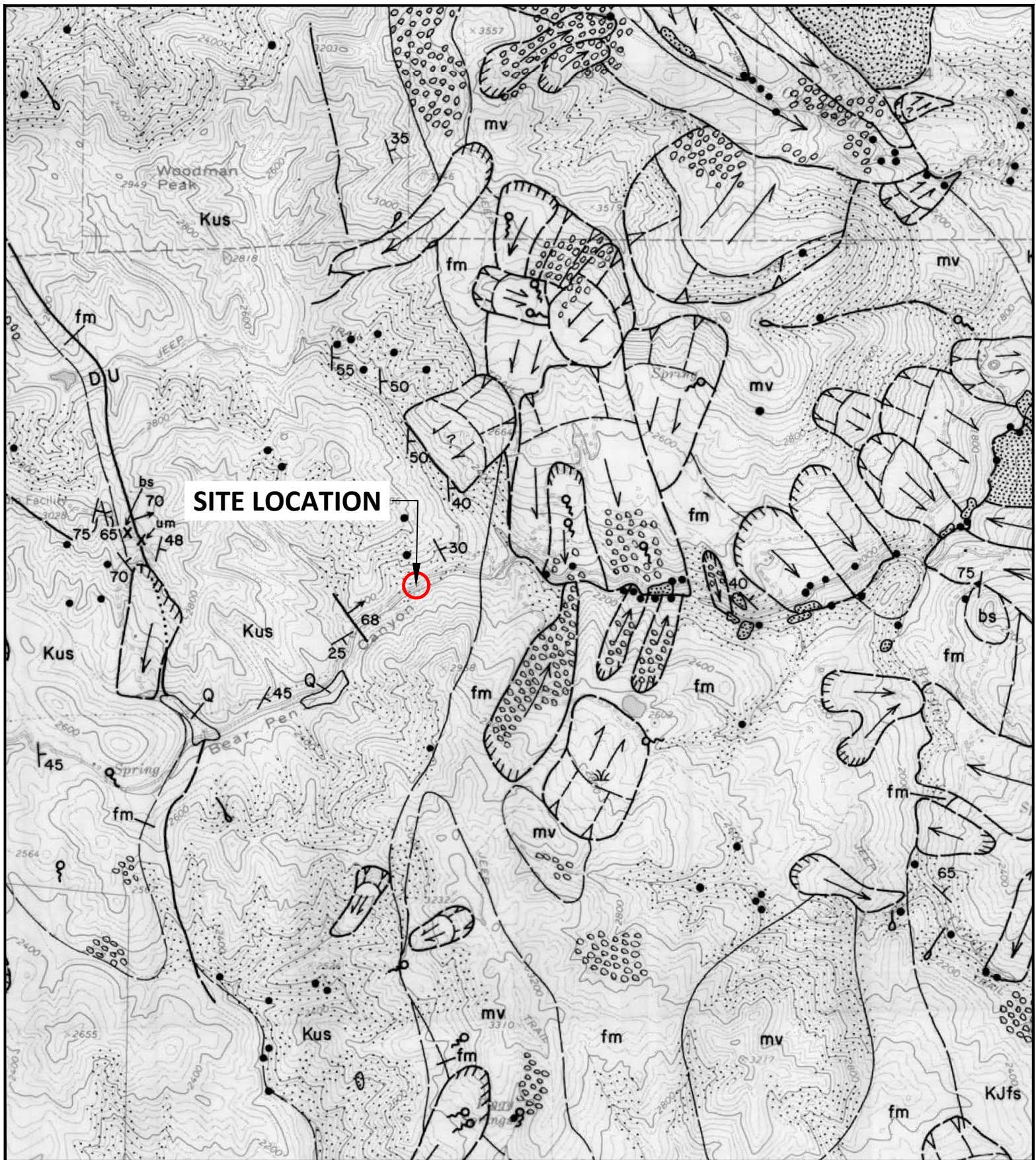
**GEOTECHNICAL INVESTIGATION  
LAYTONVILLE DOS RIOS ROAD  
(CR 322) FAILURE AT MP 3.34**

LAYTONVILLE, MENDOCINO CO., CA

**Figure 3**  
Regional  
Geologic Map

Prj. No: 16-337.10  
Scale: 1" = 10,000'  
Date: 12/15/2017





SEE FIGURE 4B FOR LEGEND



NORTH

**Map Source:**

Kilbourne, R.T., 1984, *Geology and Geomorphic Features Related to Landsliding, Laytonville 7.5' Quadrangle, OFR 84-41, California Division of Mines and Geology, Scale 1:24,000*



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**GEOTECHNICAL INVESTIGATION  
LAYTONVILLE DOS RIOS ROAD  
(CR 322) FAILURE AT MP 3.34**

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**Figure 4A**  
Landslide and  
Geologic Map

Prj. No: 16-337.10  
Scale: 1" = 2,000'  
Date: 12/15/2017





**TRANSLATIONAL/ROTATIONAL SLIDE:** relatively cohesive slide mass with a failure plane that is deep-seated in comparison to that of a debris slide of similar areal extent; sense of motion along slide plane is linear in a translational slide and arcuate or "rotational" in a rotational slide; complex versions with rotational heads and translational movement or earthflows downslope are common; translational movement along a planar joint or bedding discontinuity may be referred to as a block glide;  $\curvearrowright$  indicates scarp,  $\leftarrow$  indicates direction of movement; dashed where dormant, queried where uncertain.



**EARTHFLOW:** mass movement resulting from slow to rapid flowage of saturated soil and debris in a semiviscous, highly plastic state; after initial failure, the flow may move, or creep, seasonally in response to destabilizing forces;  $\curvearrowright$  indicates scarp,  $\leftarrow$  indicates direction of movement; dashed where dormant, queried where uncertain.



**DEBRIS SLIDE:** unconsolidated rock, colluvium, and soil that has moved slowly to rapidly downslope along a relatively steep (generally greater than 65 percent), shallow translational failure plane; forms steep, unvegetated scars in the head region and irregular hummocky deposits (when present) in the toe region; scars likely to ravel and remain unvegetated for many years; revegetated scars recognized by steep, even-faceted slope and light-bulb shape; includes scarp and slide deposits; solid where active, dashed where dormant.



**DEBRIS FLOW/TORRENT TRACK:** long stretches of bare, generally unstable stream channel banks scoured and eroded by the extremely rapid movement of water-laden debris; commonly triggered by debris sliding in the upper part of the drainage during high intensity storms; scoured debris may be deposited downslope as a tangled mass of organic material in a matrix of rock and soil; debris may be reactivated or washed away during subsequent events; solid where active, dashed where dormant.



**DEBRIS SLIDE SLOPE:** geomorphic feature characterized by steep (generally greater than 65 percent), usually well vegetated slopes that have been sculpted by numerous debris slide events; vegetated soils and colluvium above shallow soil/bedrock interface may be disrupted by active debris slides or bedrock exposed by former debris sliding; slopes near angle repose may be relatively stable except where weak bedding planes and extensive bedrock joints and fractures parallel slope.

- **ACTIVE SLIDE:** too small to delineate at this scale.



**DISRUPTED GROUND:** irregular ground surface caused by complex landsliding processes resulting in features that are indistinguishable or too small to delineate individually at this scale; also may include areas affected by downslope creep, expansive soils, and/or gully erosion; boundaries usually are indistinct.

**Q ALLUVIUM (Holocene):** unconsolidated, fine-grained sand and silt along modern river flood plains; minor amounts of gravel in channel areas.

**Qf ALLUVIAL FAN DEPOSITS (Holocene):** fan-shaped deposits of unconsolidated, poorly sorted sand and gravel; found in lowlands at the mouths of steep drainage canyons; deposits may represent material transported by debris torrents.

**Qo OLDER ALLUVIUM (Holocene-Pleistocene):** flat-lying, compact but unconsolidated river and lake deposits ranging from boulder conglomerate and breccia to fine sand and silt; coarser facies more common at base along edge of deposit near contact with upland areas of Franciscan melange (fm).

**mv VOLCANIC ROCKS:** principally greenstone; includes altered diabase, pillow basalt, and volcanic breccia; chert is commonly mixed with the volcanics.

**TKfs COASTAL BELT FRANCISCAN (Tertiary-Cretaceous):** well consolidated, folded and fractured, clastic sedimentary rocks; includes arkosic sandstone, shale, and small amounts of pebble conglomerate; sandstones commonly are laumontized.

**Kus WHITE ROCK SANDSTONE (Upper Cretaceous):** deformed, but well consolidated; includes volcanic and quartz arenite, shale, and small amounts of pebble conglomerate; sandstones commonly are laumontized, massive units that develop steep slopes; boundaries slightly modified from White Rock unit of Guwva (1974).

**fm FRANCISCAN MELANGE (Tertiary-Cretaceous):** pervasively sheared, argillaceous matrix surrounding pebble-size to individually mappable blocks of graywacke, greenstone, chert, conglomerate, serpentinite and serpentinized ultramafic rocks; the highly erodible, sheared shale matrix generally is very unstable in the Laytonville quadrangle and is prone to landsliding, even on gentle slopes; locally the melange is indistinguishable from fault gouge.

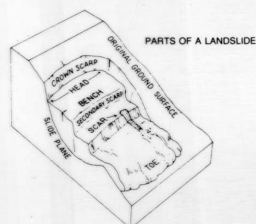
ls - limestone

um - serpentinite and ultramafic rocks

bs - glaucophane schist and blueschist

cg - conglomerate

sh - shale



**KJfs FRANCISCAN CENTRAL BELT SEDIMENTARY ROCKS (Cretaceous-Jurassic):** large, well consolidated blocks of graywacke, siltstone, mudstone, conglomerate, and small amounts of greenstone surrounded by a sheared clayey matrix; on the Laytonville and Iron Peak quadrangles this unit is lithologically the same as the Eel River melange of Guwva (1974), but is considered to be gradational with, and less sheared than, typical melange.

**LITHOLOGIC CONTACT:** dashed where approximately located.

**ROCK OUTCROP:** too small to delineate boundaries at this scale.

**FAULT:** dashed where approximately located, dotted where concealed or inferred; letters (U=Up, D=Down) and arrows indicate sense of movement; usually associated with highly sheared, landslide-prone fault gouge.

**SHEAR ZONE:** fault zone without distinctive mappable fault trace; landslide prone.

**LINEAMENT:** linear feature of unknown origin observed on aerial photographs; usually associated with erodible rock units.

**STRIKE AND DIP OF BEDDING**

**APPROXIMATE STRIKE AND DIP OF BEDDING:** appears without numerical designation or dip angle.

**STRIKE OF VERTICAL BEDDING**

**STRIKE AND DIP OF FAULT PLANE**

**STRIKE AND DIP OF FOLIATION**

**SPRING**

**MARSH OR SMALL POND**

**QUARRY OR BORROW PIT**

#### REFERENCES

California Department of Forestry, 1981, Cal Aero Photos: Photos CDF-ALL-UK; Flight 6/30/81; Frames 20-9 to 20-14, 22-8 to 22-14, 24-9 to 24-15, and 26-10 to 26-16; black and white, scale 1:24,000.

California Division of Mines and Geology, 1983, Official Map of Special Studies Zones, Laytonville quadrangle: Scale 1:24,000.

California Division of Mines and Geology, 1976-1984, Geologic review of Timber Harvesting Plans: Unpublished field studies conducted for the California Department of Forestry.

Guwva, P.R., 1974, Geology of the Covelo/Laytonville area, northern California: University of Texas at Austin, unpublished Ph.D. thesis, 82 pages, map scale 1:62,500.

Kilbourne, R.T., 1984, Geology and geomorphic features related to landsliding, Iron Peak 7.5' quadrangle, Mendocino County, California: California Department of Conservation, Division of Mines and Geology, Open File Report 84-40 PH, scale 1:24,000.

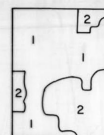
Kilbourne, R.T., 1983, Geology and geomorphic features related to landsliding, Cahto Peak 7.5' quadrangle, Mendocino County, California: California Division of Mines and Geology, Open File Report 83-39 SF, scale 1:24,000.

Kilbourne, R.T., 1984, Geology and geomorphic features related to landsliding, Longvale 7.5' quadrangle, Mendocino County, California: California Division of Mines and Geology, Open File Report 84-18 SF, scale 1:24,000.

#### SOURCES OF GEOLOGIC DATA

Geologic data were compiled from aerial photo interpretation, field reconnaissance, and the modification of unpublished geologic data from references listed above. The author was assisted in the field and office studies by Dan Trumbly and Lydia Lofgren.

1. Mapping from aerial photo interpretation, previously existing geologic data, and reconnaissance level field work.
2. Mapping from aerial photo interpretation and previously existing geologic data.



#### ACTIVITY OF LANDSLIDES

Active or probably active - presently moving or recently moved. Distinct topographic slide features present, i.e., sharp barren scarps, cracks, jackstrawed trees. Major revegetation has not occurred.

Dormant - little evidence of recent movement. Slide features modified by weathering and erosion. Vegetation generally well established. Some mass movements may have developed under climatic conditions different from today. Causes of failure may remain and movement could be renewed.

#### RATES OF LANDSLIDE MOVEMENT\*

10 ft/sec or more	= extremely rapid
1 ft/min-10 ft/sec	= very rapid
5 ft/day-1 ft/min	= rapid
5 ft/mo-5 ft/day	= moderate
5 ft/yr-5 ft/mo	= slow
1 ft/yr-5 ft/yr	= very slow
1 ft/yr or less	= extremely slow

\*Modified from: Varnes, D.J., 1978, Slope movement types and processes, in Landslides: Analysis and Control, Transportation Research Board, National Academy of Sciences, Washington, D.C., Special Report 176, Figure 2.1.

## SEE FIGURE 4A FOR MAP

#### Map Source:

Kilbourne, R.T., 1984, Geology and Geomorphic Features Related to Landsliding, Laytonville 7.5' Quadrangle, OFR 84-41, California Division of Mines and Geology, Scale 1:24,000

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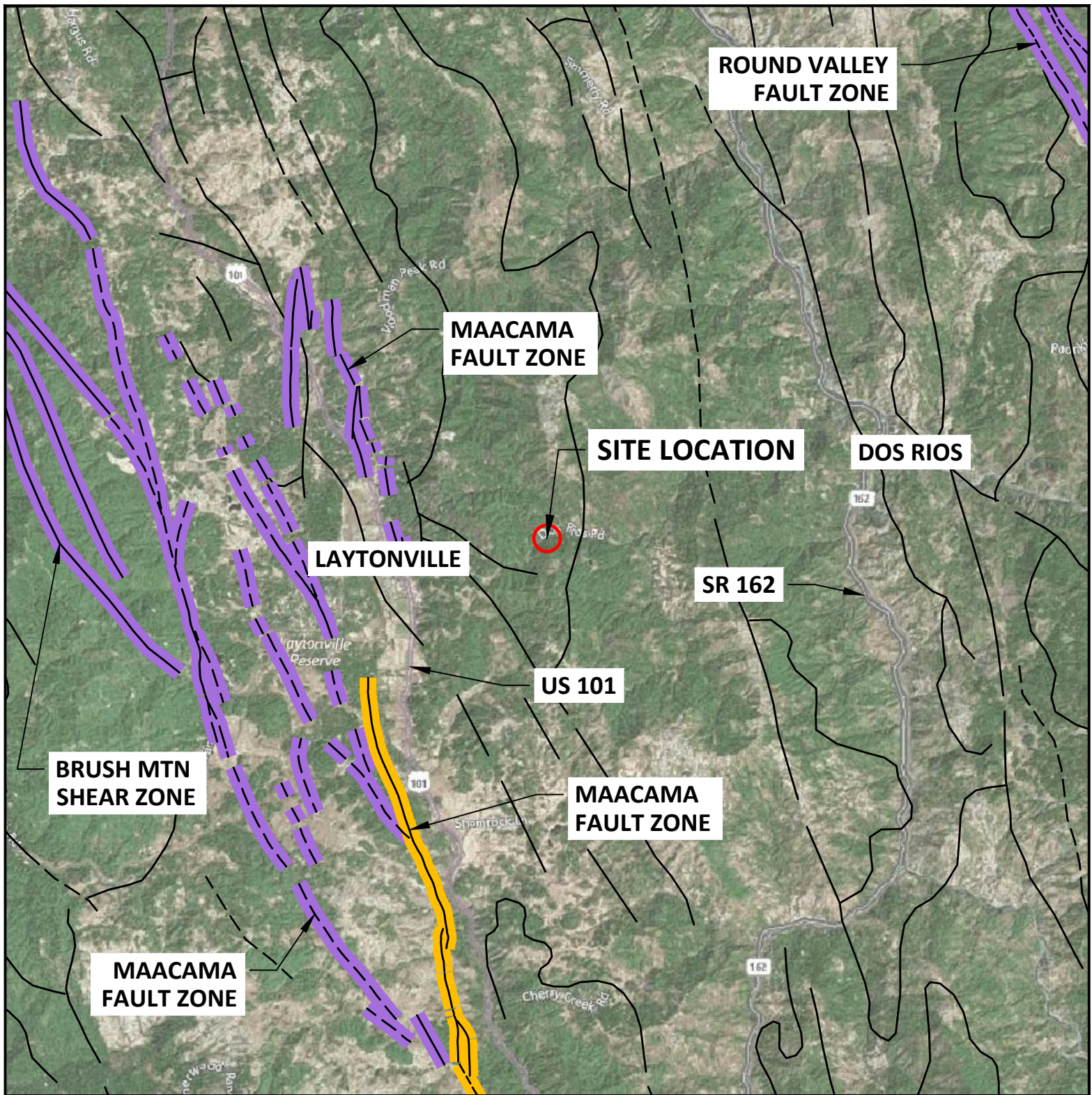
GEOTECHNICAL INVESTIGATION  
LAYTONVILLE DOS RIOS ROAD  
(CR 322) FAILURE AT MP 3.34  
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#### Figure 4B Landslide and Geologic Map Legend

Prj. No: 16-337.10  
Scale: N/A  
Date: 12/15/2017

NORTH





## LEGEND

### CGS Faults (Last Activity Age)

- <200 years (Historic)
- <11,700 years (Holocene)
- <700,000 years (Late Quaternary)

### CGS Faults (Last Activity Age)

- <1.6 million years (Quaternary)
- >1.6 million years (Pre-Quaternary)

### Fault Location

- Certain
- - - Approx. or Inferred
- Concealed



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### Map and Data Sources:

1. Basemap via AutoCAD Civil 3D geolocation tool
2. Fault data via CGS Fault Activity Map of California 2010 GIS data



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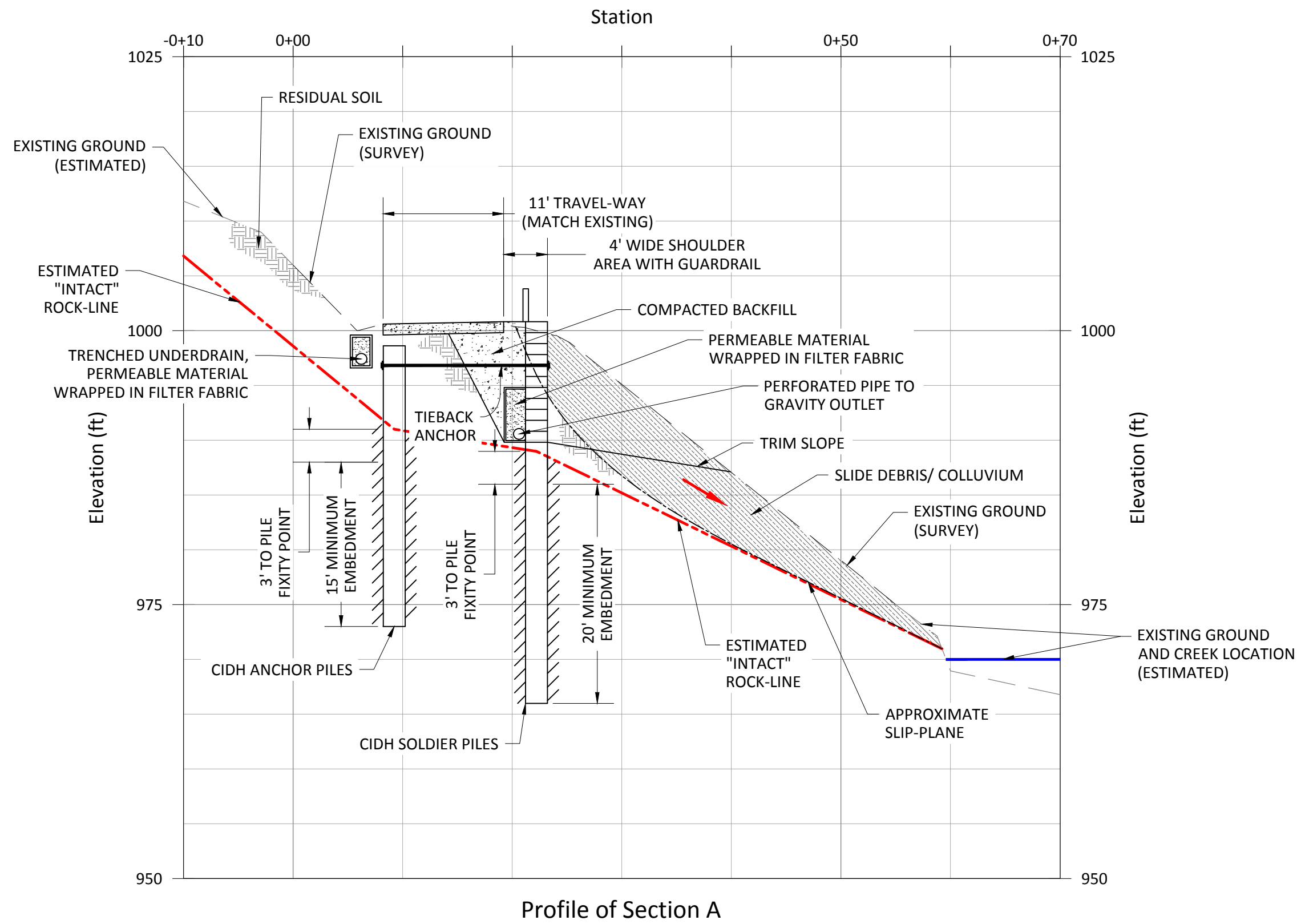
GEOTECHNICAL INVESTIGATION  
LAYTONVILLE DOS RIOS ROAD  
(CR 322) FAILURE AT MP 3.34

LAYTONVILLE, MENDOCINO CO., CA

**Figure 5**  
Fault Activity  
Map

Prj. No: 16-337.10  
Scale: 1" = 10,000'  
Date: 12/15/2017





NORTH

**Data Source:**  
Existing Topography provided by MCDOT via electronic transfer on 10/31/2017. Survey completed by MCDOT.

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**Figure 6**  
Typical Section of Soldier Pile Tieback Wall  
Prj. No: 16-337.10  
Scale: 1" = 10'  
Date: 03/08/2018

Path: \\psf\home\Box\Projects\16-337.X Mendocino 2016 Quadrennial Support Project\16-337.10 Laytonville Dos Rios Road (CR 322) at MP 3.34, 3.66, and 4.19\CAD\16-337.10-Figures-MP 3.34.dwg Plot Date: Mar 13, 2018 at 1:37pm



**GEOTECHNICAL MEMORANDUM**

Laytonville Dos Rios Road (CR 322) Failure at MP 3.34

CAI File: 16-337.10

April 23, 2018

**APPENDIX A**

**BORING LOG LEGEND**

**BORING LOGS**



## GROUP SYMBOLS AND NAMES

Graphic / Symbol	Group Names	Graphic / Symbol	Group Names
	Well-graded GRAVEL Well-graded GRAVEL with SAND		Lean CLAY Lean CLAY with SAND Lean CLAY with GRAVEL SANDY lean CLAY SANDY lean CLAY with GRAVEL GRAVELLY lean CLAY GRAVELLY lean CLAY with SAND
	Poorly graded GRAVEL Poorly graded GRAVEL with SAND		SILTY CLAY SILTY CLAY with SAND SILTY CLAY with GRAVEL SANDY SILTY CLAY SANDY SILTY CLAY with GRAVEL GRAVELLY SILTY CLAY GRAVELLY SILTY CLAY with SAND
	Well-graded GRAVEL with SILT Well-graded GRAVEL with SILT and SAND		SILT SILT with SAND SILT with GRAVEL SANDY SILT SANDY SILT with GRAVEL GRAVELLY SILT GRAVELLY SILT with SAND
	Well-graded GRAVEL with CLAY (or SILTY CLAY) (or SILTY CLAY and SAND)		ORGANIC lean CLAY ORGANIC lean CLAY with SAND ORGANIC lean CLAY with GRAVEL SANDY ORGANIC lean CLAY SANDY ORGANIC lean CLAY with GRAVEL GRAVELLY ORGANIC lean CLAY GRAVELLY ORGANIC lean CLAY with SAND
	Poorly graded GRAVEL with SILT Poorly graded GRAVEL with SILT and SAND		ORGANIC lean CLAY ORGANIC lean CLAY with SAND ORGANIC lean CLAY with GRAVEL SANDY ORGANIC lean CLAY SANDY ORGANIC lean CLAY with GRAVEL GRAVELLY ORGANIC lean CLAY GRAVELLY ORGANIC lean CLAY with SAND
	Poorly graded GRAVEL with CLAY (or SILTY CLAY) Poorly graded GRAVEL with CLAY and SAND (or SILTY CLAY and SAND)		ORGANIC lean CLAY ORGANIC lean CLAY with SAND ORGANIC lean CLAY with GRAVEL SANDY ORGANIC lean CLAY SANDY ORGANIC lean CLAY with GRAVEL GRAVELLY ORGANIC lean CLAY GRAVELLY ORGANIC lean CLAY with SAND
	SILTY GRAVEL SILTY GRAVEL with SAND		ORGANIC lean CLAY ORGANIC lean CLAY with SAND ORGANIC lean CLAY with GRAVEL SANDY ORGANIC lean CLAY SANDY ORGANIC lean CLAY with GRAVEL GRAVELLY ORGANIC lean CLAY GRAVELLY ORGANIC lean CLAY with SAND
	CLAYEY GRAVEL CLAYEY GRAVEL with SAND		ORGANIC lean CLAY ORGANIC lean CLAY with SAND ORGANIC lean CLAY with GRAVEL SANDY ORGANIC lean CLAY SANDY ORGANIC lean CLAY with GRAVEL GRAVELLY ORGANIC lean CLAY GRAVELLY ORGANIC lean CLAY with SAND
	SILTY, CLAYEY GRAVEL SILTY, CLAYEY GRAVEL with SAND		ORGANIC lean CLAY ORGANIC lean CLAY with SAND ORGANIC lean CLAY with GRAVEL SANDY ORGANIC lean CLAY SANDY ORGANIC lean CLAY with GRAVEL GRAVELLY ORGANIC lean CLAY GRAVELLY ORGANIC lean CLAY with SAND
	Well-graded SAND Well-graded SAND with GRAVEL		Fat CLAY Fat CLAY with SAND Fat CLAY with GRAVEL SANDY fat CLAY SANDY fat CLAY with GRAVEL GRAVELLY fat CLAY GRAVELLY fat CLAY with SAND
	Poorly graded SAND Poorly graded SAND with GRAVEL		Elastic SILT Elastic SILT with SAND Elastic SILT with GRAVEL SANDY elastic SILT SANDY elastic SILT with GRAVEL GRAVELLY elastic SILT GRAVELLY elastic SILT with SAND
	Well-graded SAND with SILT Well-graded SAND with SILT and GRAVEL		ORGANIC fat CLAY ORGANIC fat CLAY with SAND ORGANIC fat CLAY with GRAVEL SANDY ORGANIC fat CLAY SANDY ORGANIC fat CLAY with GRAVEL GRAVELLY ORGANIC fat CLAY GRAVELLY ORGANIC fat CLAY with SAND
	Well-graded SAND with CLAY (or SILTY CLAY) (or SILTY CLAY and GRAVEL)		ORGANIC elastic SILT ORGANIC elastic SILT with SAND ORGANIC elastic SILT with GRAVEL SANDY elastic ELASTIC SILT SANDY ORGANIC elastic SILT with GRAVEL GRAVELLY ORGANIC elastic SILT GRAVELLY ORGANIC elastic SILT with SAND
	Poorly graded SAND with SILT Poorly graded SAND with SILT and GRAVEL		ORGANIC elastic SILT ORGANIC elastic SILT with SAND ORGANIC elastic SILT with GRAVEL SANDY elastic ELASTIC SILT SANDY ORGANIC elastic SILT with GRAVEL GRAVELLY ORGANIC elastic SILT GRAVELLY ORGANIC elastic SILT with SAND
	Poorly graded SAND with CLAY (or SILTY CLAY) (or SILTY CLAY and GRAVEL)		ORGANIC elastic SILT ORGANIC elastic SILT with SAND ORGANIC elastic SILT with GRAVEL SANDY elastic ELASTIC SILT SANDY ORGANIC elastic SILT with GRAVEL GRAVELLY ORGANIC elastic SILT GRAVELLY ORGANIC elastic SILT with SAND
	SILTY SAND SILTY SAND with GRAVEL		ORGANIC elastic SILT ORGANIC elastic SILT with SAND ORGANIC elastic SILT with GRAVEL SANDY elastic ELASTIC SILT SANDY ORGANIC elastic SILT with GRAVEL GRAVELLY ORGANIC elastic SILT GRAVELLY ORGANIC elastic SILT with SAND
	CLAYEY SAND CLAYEY SAND with GRAVEL		ORGANIC elastic SILT ORGANIC elastic SILT with SAND ORGANIC elastic SILT with GRAVEL SANDY elastic ELASTIC SILT SANDY ORGANIC elastic SILT with GRAVEL GRAVELLY ORGANIC elastic SILT GRAVELLY ORGANIC elastic SILT with SAND
	SILTY, CLAYEY SAND SILTY, CLAYEY SAND with GRAVEL		ORGANIC elastic SILT ORGANIC elastic SILT with SAND ORGANIC elastic SILT with GRAVEL SANDY elastic ELASTIC SILT SANDY ORGANIC elastic SILT with GRAVEL GRAVELLY ORGANIC elastic SILT GRAVELLY ORGANIC elastic SILT with SAND
	PEAT		ORGANIC SOIL ORGANIC SOIL with SAND ORGANIC SOIL with GRAVEL SANDY ORGANIC SOIL SANDY ORGANIC SOIL with GRAVEL GRAVELLY ORGANIC SOIL GRAVELLY ORGANIC SOIL with SAND
	COBBLES COBBLES and BOULDERS BOULDERS		ORGANIC SOIL ORGANIC SOIL with SAND ORGANIC SOIL with GRAVEL SANDY ORGANIC SOIL SANDY ORGANIC SOIL with GRAVEL GRAVELLY ORGANIC SOIL GRAVELLY ORGANIC SOIL with SAND

## FIELD AND LABORATORY TESTS

<b>C</b>	Consolidation (ASTM D 2435)
<b>CL</b>	Collapse Potential (ASTM D 4546)
<b>CP</b>	Compaction Curve (CTM 216)
<b>CR</b>	Corrosion, Sulfates, Chlorides (CTM 643, CTM 417, CTM 422)
<b>CU</b>	Consolidated Undrained Triaxial (ASTM D 4767)
<b>DR</b>	Drained Residual Shear Strength (ASTM D 6467)
<b>DS</b>	Direct Shear (ASTM D 3080)
<b>EI</b>	Expansion Index (ASTM D 4829)
<b>M</b>	Moisture Content (ASTM D 2216)
<b>OC</b>	Organic Content (ASTM D 2974)
<b>P</b>	Permeability (CTM 220)
<b>PA</b>	Particle Size Analysis (ASTM D 422)
<b>PI</b>	Liquid Limit, Plastic Limit, Plasticity Index (AASHTO T 89, AASHTO T 90)
<b>PL</b>	Point Load Index (ASTM D 5731)
<b>PM</b>	Pressure Meter
<b>R</b>	R-Value (CTM 301)
<b>SE</b>	Sand Equivalent (CTM 217)
<b>SG</b>	Specific Gravity (AASHTO T 100)
<b>SW</b>	Swell Potential (ASTM D 4546)
<b>UC</b>	Unconfined Compression - Soil (ASTM D 2166) Unconfined Compression - Rock (ASTM D 7012-C)
<b>UU</b>	Unconsolidated Undrained Triaxial (ASTM D 2850)
<b>UW</b>	Unit Weight (ASTM D 7263)

## SAMPLER GRAPHIC SYMBOLS

	Standard Penetration Test (SPT)
	Standard California Sampler (ID 2.5 in.)
	Modified California Sampler (ID 2.0 in.)
	Shelby Tube
	Piston Sampler
	NX Rock Core
	HQ Rock Core
	Bulk Sample
	Other (see remarks)

## DRILLING METHOD SYMBOLS

	Auger Drilling		Rotary Drilling		Dynamic Cone or Hand Driven		Diamond Core
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## WATER LEVEL SYMBOLS

	First Water Level Reading (during drilling)
	Static Water Level Reading (short-term)
	Static Water Level Reading (long-term)

**REFERENCE:** Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010) with Errata Sheet (2015).



### CONSISTENCY OF COHESIVE SOILS

Descriptor	Unconfined Compressive Strength (tsf)	Pocket Penetrometer (tsf)	Torvane (tsf)	Field Approximation
Very Soft	< 0.25	< 0.25	< 0.12	Easily penetrated several inches by fist
Soft	0.25 - 0.50	0.25 - 0.50	0.12 - 0.25	Easily penetrated several inches by thumb
Medium Stiff	0.50 - 1.0	0.50 - 1.0	0.25 - 0.50	Can be penetrated several inches by thumb with moderate effort
Stiff	1.0 - 2.0	1.0 - 2.0	0.50 - 1.0	Readily indented by thumb but penetrated only with great effort
Very Stiff	2.0 - 4.0	2.0 - 4.0	1.0 - 2.0	Readily indented by thumbnail
Hard	> 4.0	> 4.0	> 2.0	Indented by thumbnail with difficulty

### APPARENT DENSITY OF COHESIONLESS SOILS

Descriptor	SPT N <sub>60</sub> (blows / 12 inches)
Very Loose	0 - 5
Loose	5 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	> 50

### MOISTURE

Descriptor	Criteria
Dry	No discernable moisture
Moist	Moisture present, but no free water
Wet	Visible free water

### PERCENT OR PROPORTION OF SOILS

Descriptor	Criteria
Trace	Particles are present but estimated to be less than 5%
Few	5 to 10%
Little	15 to 25%
Some	30 to 45%
Mostly	50 to 100%

### SOIL PARTICLE SIZE

Descriptor		Size
Boulder		> 12 inches
Cobble		3 to 12 inches
Gravel	Coarse	3/4 inch to 3 inches
	Fine	No. 4 Sieve to 3/4 inch
Sand	Coarse	No. 10 Sieve to No. 4 Sieve
	Medium	No. 40 Sieve to No. 10 Sieve
	Fine	No. 200 Sieve to No. 40 Sieve
Silt and Clay		Passing No. 200 Sieve

### PLASTICITY OF FINE-GRAINED SOILS

Descriptor	Criteria
Nonplastic	A 1/8-inch thread cannot be rolled at any water content.
Low	The thread can barely be rolled, and the lump cannot be formed when drier than the plastic limit.
Medium	The thread is easy to roll, and not much time is required to reach the plastic limit; it cannot be rerolled after reaching the plastic limit. The lump crumbles when drier than the plastic limit.
High	It takes considerable time rolling and kneading to reach the plastic limit. The thread can be rerolled several times after reaching the plastic limit. The lump can be formed without crumbling when drier than the plastic limit.

### CEMENTATION

Descriptor	Criteria
Weak	Crumbles or breaks with handling or little finger pressure.
Moderate	Crumbles or breaks with considerable finger pressure.
Strong	Will not crumble or break with finger pressure.

**REFERENCE:** Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010).



### ROCK GRAPHIC SYMBOLS



IGNEOUS ROCK



SEDIMENTARY ROCK



METAMORPHIC ROCK

### BEDDING SPACING

Descriptor	Thickness or Spacing
Massive	> 10 ft
Very thickly bedded	3 ft - 10 ft
Thickly bedded	1 ft - 3 ft
Moderately bedded	4 in - 1 ft
Thinly bedded	1 in - 4 in
Very thinly bedded	1/4 in - 1 in
Laminated	< 1/4 in

### WEATHERING DESCRIPTORS FOR INTACT ROCK

	Diagnostic Features					
Descriptor	Chemical Weathering-Discoloration-Oxidation		Mechanical Weathering and Grain Boundary Conditions	Texture and Solutioning		General Characteristics
	Body of Rock	Fracture Surfaces		Texture	Solutioning	
Fresh	No discoloration, not oxidized	No discoloration or oxidation	No separation, intact (tight)	No change	No solutioning	Hammer rings when crystalline rocks are struck.
Slightly Weathered	Discoloration or oxidation is limited to surface of, or short distance from, fractures; some feldspar crystals are dull	Minor to complete discoloration or oxidation of most surfaces	No visible separation, intact (tight)	Preserved	Minor leaching of some soluble minerals may be noted	Hammer rings when crystalline rocks are struck. Body of rock not weakened.
Moderately Weathered	Discoloration or oxidation extends from fractures usually throughout; Fe-Mg minerals are "rusty"; feldspar crystals are "cloudy"	All fracture surfaces are discolored or oxidized	Partial separation of boundaries visible	Generally preserved	Soluble minerals may be mostly leached	Hammer does not ring when rock is struck. Body of rock is slightly weakened.
Intensely Weathered	Discoloration or oxidation throughout; all feldspars and Fe-Mg minerals are altered to clay to some extent; or chemical alteration produces in situ disaggregation (refer to grain boundary conditions)	All fracture surfaces are discolored or oxidized; surfaces are friable	Partial separation, rock is friable; in semi-arid conditions, granitics are disaggregated	Altered by chemical disintegration such as via hydration or argillation	Leaching of soluble minerals may be complete	Dull sound when struck with hammer; usually can be broken with moderate to heavy manual pressure or by light hammer blow without reference to planes of weakness such as incipient or hairline fractures or veinlets. Rock is significantly weakened.
Decomposed	Discolored or oxidized throughout, but resistant minerals such as quartz may be unaltered; all feldspars and Fe-Mg minerals are completely altered to clay		Complete separation of grain boundaries (disaggregated)	Resembles a soil; partial or complete remnant rock structure may be preserved; leaching of soluble minerals usually complete		Can be granulated by hand. Resistant minerals such as quartz may be present as "stringers" or "dikes".

**Note:** Combination descriptors (such as "slightly weathered to fresh") are used where equal distribution of both weathering characteristics is present over significant intervals or where characteristics present are "in between" the diagnostic feature. However, combination descriptors should not be used where significant identifiable zones can be delineated. Only two adjacent descriptors shall be combined. "Very intensely weathered" is the combination descriptor for "decomposed to intensely weathered".

### PERCENT CORE RECOVERY (REC)

$$\frac{\sum \text{Length of the recovered core pieces (in.)}}{\text{Total length of core run (in.)}} \times 100$$

### ROCK QUALITY DESIGNATION (RQD)

$$\frac{\sum \text{Length of intact core pieces} > 4 \text{ in.}}{\text{Total length of core run (in.)}} \times 100$$

**Note:** RQD\* indicates soundness criteria not met

### ROCK HARDNESS

Descriptor	Criteria
Extremely Hard	Specimen cannot be scratched with pocket knife or sharp pick; can only be chipped with repeated heavy hammer blows
Very hard	Specimen cannot be scratched with pocket knife or sharp pick; breaks with repeated heavy hammer blows
Hard	Specimen can be scratched with pocket knife or sharp pick with heavy pressure; heavy hammer blows required to break specimen
Moderately Hard	Specimen can be scratched with pocket knife or sharp pick with light or moderate pressure; breaks with moderate hammer blows
Moderately Soft	Specimen can be grooved 1/16 in. with pocket knife or sharp pick with moderate or heavy pressure; breaks with light hammer blow or heavy hand pressure
Soft	Specimen can be grooved or gouged with pocket knife or sharp pick with light pressure, breaks with light to moderate hand pressure
Very Soft	Specimen can be readily indented, grooved, or gouged with fingernail, or carved with pocket knife; breaks with light manual pressure.

### FRACTURE DENSITY

Descriptor	Criteria
Unfractured	No fractures
Very Slightly Fractured	Core lengths greater than 3 ft.
Slightly Fractured	Core lengths mostly from 1 ft. to 3 ft.
Moderately Fractured	Core lengths mostly from 4 in. to 1 ft.
Intensely Fractured	Core lengths mostly from 1 in. to 4 in.
Very Intensely Fractured	Mostly chips and fragments.

**REFERENCE:** Caltrans Soil and Rock Logging, Classification, and Presentation Manual (2010).



## LOG OF BORING B1

PROJECT NO: 16-337.10

PROJECT: Laytonville Dos Rios Rd. MP 3.34

LOCATION: L.D.R. Rd. (CR 322), Laytonville

CITY/COUNTY: Mendocino

CLIENT: MCDOT

LOGGED BY: EET

DEPTH OF BORING: 35.08 (ft)

BEGIN DATE: 1/18/18

COMPLETION DATE: 1/18/18

SURFACE ELEVATION: 1001.4 (ft)\*

SURFACE CONDITION: Dirt/Gravel

WATER DEPTH: 24 (ft)

READING TAKEN: 1/18/18

HAMMER EFFICIENCY: 80 (%)

DRILLING CONTRACTOR: Clear Heart Drilling, Inc.

DRILLING METHOD: Hollow-Stem Auger (6" OD, 2.25" ID)

DRILL RIG: Deeprock - DR5K (Truck)

HAMMER TYPE: Automatic, 140 lbs, 30" drop

SAMPLER TYPE & SIZE: SPT (ID 1.4")

BOREHOLE DIAMETER: 6"

BACKFILL METHOD: Type II-V Portland Cement

FIELD						GRAPHIC LOG	DESCRIPTION	RECOVERY (%)	LABORATORY						REMARKS
ELEV (ft)	DEPTH (ft)	SAMPLE	SAMPLE NO	BLOWS PER 6 INCH	BLOWS PER FOOT	POCKET PEN. (TSF)			RQD (%)	LIQUID LIMIT	PLASTIC LIMIT	MOISTURE (%)	D. DENSITY (PCF)	% PASSING 200 SIEVE	
1000	1		0				SILTY SAND (SM); brown; about 10% coarse to fine GRAVEL; coarse to fine SAND; nonplastic fines [FILL].	100						22	
998	2														
	3														
996	4														
	5		1	2	2		Very loose to loose.	22							
	6			1											
	7			1											
994	8														
	9						SEDIMENTARY ROCK (SANDSTONE), light brown, intensely weathered, dry to moist [UNDIVIDED MARINE FORMATION].								Driller reported material change at 8'
992	10		2	50/6"	REF	3.50		100				7.9	90.2		
	11														
990	12														
	13														
988	14														
	15		3	50/2"	REF		Intensely to moderately weathered, dry.	100							Heavy drill rig "chatter" at 15'
986	16														
	17														
984	18														
	19														
982	20		4	50/1"	REF		Dark gray.	100							Very slow auger progression at 20'
	21														
980	22														
	23														Easier drilling at 23'
978															



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Sacramento, CA 95831  
(916) 455-4225

PROJECT NUMBER: 16-337.10  
PROJECT: Laytonville Dos Rios Rd. MP 3.34  
BORING: B1  
ENTRY BY: RRR  
CHECKED BY: RDS  
SHEET 1 of 2



FIELD							GRAPHIC LOG	DESCRIPTION	RECOVERY (%)	RQD (%)	LABORATORY						DRILL METHOD	CASING DEPTH	REMARKS
ELEV (ft)	DEPTH (ft)	SAMPLE	SAMPLE NO	BLOWS PER 6 INCH	BLOWS PER FOOT	POCKET PEN. (TSF)					LIQUID LIMIT	PLASTIC LIMIT	MOISTURE (%)	D. DENSITY (PCF)	% PASSING 200 SIEVE				
976	25		5	50/0"	REF												Hard drilling, rig "chatter" at 25'		
	26																		
974	27																Initial groundwater at 30.2'		
	28																		
972	29																		
	30		6	50/2"	REF														
970	31																		
	32																		
968	33																		
	34																		
966	35		7	50/1"	REF												Auger refusal at 35'		
	36																		
964	37																Backfilled with 94lbs bags of portland cement grout (mix 5 bags/50 gal. water)		
	38																		
962	39																*Elevation Reference: CP 1, Elev. 1000.00 feet per MCDOT topographic survey		
	40																		
960	41																		
	42																		
958	43																		
	44																		
956	45																		
	46																		
954	47																		
	48																		
952	49																		
	50																		
950	51																		
	52																		
953	53																		



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PROJECT NUMBER: 16-337.10  
PROJECT: Laytonville Dos Rios Rd. MP 3.34  
BORING: B1  
ENTRY BY: RRH  
CHECKED BY: RDS  
SHEET 2 of 2



## LOG OF BORING B2

PROJECT NO: 16-337.10

PROJECT: Laytonville Dos Rios Rd. MP 3.34

LOCATION: L.D.R. Rd. (CR 322), Laytonville

CITY/COUNTY: Mendocino

CLIENT: MCDOT

LOGGED BY: EET

DEPTH OF BORING: 37.04 (ft)

BEGIN DATE: 1/19/18

COMPLETION DATE: 1/19/18

SURFACE ELEVATION: 1000.7 (ft)\*

SURFACE CONDITION: Dirt/Gravel

WATER DEPTH: Not Enco

READING TAKEN: 1/19/18

DRILLING CONTRACTOR: Clear Heart Drilling, Inc.

DRILLING METHOD: Hollow-Stem Auger (6" OD, 2.25" ID)

DRILL RIG: Deeprock - DR5K (Truck)

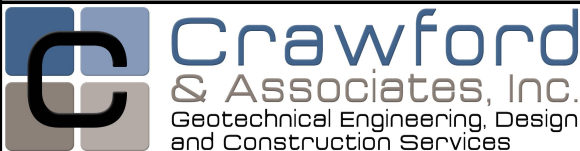
HAMMER TYPE: Automatic, 140 lbs, 30" drop

SAMPLER TYPE & SIZE: SPT (ID 1.4")

BOREHOLE DIAMETER: 6"

BACKFILL METHOD: Type II-V Portland Cement

FIELD							GRAPHIC LOG	DESCRIPTION	RECOVERY(%)	RQD (%)	LABORATORY						DRILL METHOD	CASING DEPTH	REMARKS
ELEV (ft)	DEPTH (ft)	SAMPLE	SAMPLE NO	BLOWS PER 6 INCH	BLOWS PER FOOT	POCKET PEN. (TSF)					LIQUID LIMIT	PLASTIC LIMIT	MOISTURE (%)	D. DENSITY (PCF)	% PASSING 200 SIEVE				
1000	1		0					SILTY SAND (SM); brown; moist; trace GRAVEL; coarse to fine SAND; nonplastic fines [FILL].	100	21	18			22			Chemical Analysis pH = 6.70 Min. Res. = 270 ohm-cm Chloride = 442.2 ppm Sulfate = 86.7 ppm		
998	2																		
	3																		
	4																		
996	5		1	2	5			CLAYEY SAND (SC); loose; brown; dry to moist; coarse to fine SAND; low plasticity fines.	44			6.3	108.8						
	6		2																
			3																
994	7															Driller reported material change at 9'			
	8																		
	9																		
	10																		
990	11		2	50/3"	REF				100										
	12																		
	13																		
	14																		
988	15																		
	16																		
	17																		
	18																		
986	19		3	50/2"	REF			Gray and white, intensely weathered.	0							Drill rig "chatter" at 18'			
	20																		
	21																		
	22																		
980	23		4	50/2"	REF			Dark gray, intensely to moderately weathered, dry.	0							Slow auger progression at 23'			



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PROJECT NUMBER: 16-337.10  
PROJECT: Laytonville Dos Rios Rd. MP 3.34  
BORING: B2  
ENTRY BY: RRH  
CHECKED BY: RDS SHEET 1 of 2



ELEV (ft)	DEPTH (ft)	FIELD					GRAPHIC LOG	DESCRIPTION	RECOVERY (%)	LABORATORY						CASING DEPTH	REMARKS
		SAMPLE	SAMPLE NO	BLOWS PER 6 INCH	BLOWS PER FOOT	POCKET PEN. (TSF)				RQD (%)	LIQUID LIMIT	PLASTIC LIMIT	MOISTURE (%)	D. DENSITY (PCF)	% PASSING 200 SIEVE		
976	25		5	50/3.5"	REF			Dark brown with some white, intensely weathered, dry to moist.	100								
974	26																
	27																
	28																
972	29																
	30		6	50/4"	REF			Moist, with interbedding of decomposed rock.	100				8.4	114.1			
970	31																
	32																
968	33																
	34																
966	35		7	50/1"	REF				0								
	36																
964	37		8	50/0.5"	REF			Bottom of borehole at 37.0 ft bgs	0								Auger refusal at 37'
	38							Backfilled with 94lbs bags of portland cement grout (mix 5.5 bags/55 gal. water)									
962	39							*Elevation Reference: CP 1, Elev. 1000.00 feet per MCDOT topographic survey									
	40																
960	41																
	42																
958	43																
	44																
956	45																
	46																
954	47																
	48																
952	49																
	50																
950	51																
	52																
948	53																



## LOG OF BORING B3

PROJECT NO: 16-337.10

PROJECT: Laytonville Dos Rios Rd. MP 3.34

LOCATION: L.D.R. Rd. (CR 322), Laytonville

CITY/COUNTY: Mendocino

CLIENT: MCDOT

LOGGED BY: EET

DEPTH OF BORING: 36.04 (ft)

BEGIN DATE: 1/18/18

COMPLETION DATE: 1/18/18

SURFACE ELEVATION: 1000.4 (ft)\*

SURFACE CONDITION: Dirt/Gravel

WATER DEPTH: Not Encountered (ft)

READING TAKEN: 1/18/18

HAMMER EFFICIENCY: 80 (%)

DRILLING CONTRACTOR: Clear Heart Drilling, Inc.

DRILLING METHOD: Hollow-Stem Auger (6" OD, 2.25" ID)

DRILL RIG: Deeprock - DR5K (Truck)

HAMMER TYPE: Automatic, 140 lbs, 30" drop

SAMPLER TYPE & SIZE: SPT (ID 1.4")

BOREHOLE DIAMETER: 6"

BACKFILL METHOD: Type II-V Portland Cement

FIELD						GRAPHIC LOG	DESCRIPTION	RECOVERY (%)	RQD (%)	LABORATORY						DRILL METHOD	CASING DEPTH	REMARKS
ELEV (ft)	DEPTH (ft)	SAMPLE	SAMPLE NO	BLOWS PER 6 INCH	BLOWS PER FOOT	POCKET PEN. (TSF)				LIQUID LIMIT	PLASTIC LIMIT	MOISTURE (%)	D. DENSITY (PCF)	% PASSING 200 SIEVE				
1000	1		0				CLAYEY SAND (SC); brown; moist; coarse to fine SAND; medium plasticity fines [FILL].	100		26	18			34				
998	2																	
	3																	
996	4																	
	5		1	5	12		Medium dense; trace fine GRAVEL.	6										
	6			5														
994	7			7														
	8																	
992	9						Poorly graded GRAVEL with CLAY (GP-GC); loose; brown; dry; with fractured rock [DECOMPOSED BEDROCK].											
	10		2	4	7			56				4.1	100.1	11				
990	11			4														
	12			3		3.00												
988	13																	
	14						SEDIMENTARY ROCK (SANDSTONE), brown to dark brown, intensely weathered, dry to moist [UNDIVIDED MARINE FORMATION].											
986	15		3	50/5"	REF			100				8.3	129.1					
	16																	
984	17																	
	18																	
982	19																	
	20		4	50/1"	REF		Moist.	100										
980	21																	Driller reports solid rock at 21'
	22																	
978	23																	



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PROJECT NUMBER: 16-337.10  
PROJECT: Laytonville Dos Rios Rd. MP 3.34  
BORING: B3  
ENTRY BY: RRH  
CHECKED BY: RDS  
SHEET 1 of 2



ELEV (ft)	DEPTH (ft)	FIELD					GRAPHIC LOG	DESCRIPTION	RECOVERY (%)	RQD (%)	LABORATORY						REMARKS
		SAMPLE	SAMPLE NO	BLOWS PER 6 INCH	BLOWS PER FOOT	POCKET PEN. (TSF)					LIQUID LIMIT	PLASTIC LIMIT	MOISTURE (%)	D. DENSITY (PCF)	% PASSING 200 SIEVE	DRILL METHOD	
976	25		5	50/0.5"	REF			SEDIMENTARY ROCK (Sandstone) (continued). Dark brown.	100								Heavy drill rig "chatter" at 25'
974	26																
	27																
	28																
972	29																
	30																
970	31																
	32																
968	33																
	34																
966	35		6	50/0.5"	REF			Gray, moderately weathered.	100								
	36		7	50/0.5"	REF			Bottom of borehole at 36.0 ft bgs	0								Auger refusal at 36'
964	37							Backfilled with 94lbs bags of portland cement grout (mix 5 bags/50 gal. water)									
	38							*Elevation Reference: CP 1, Elev. 1000.00 feet per MCDOT topographic survey									
962	39																
	40																
960	41																
	42																
958	43																
	44																
956	45																
	46																
954	47																
	48																
952	49																
	50																
950	51																
	52																
948	53																



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BORING: B3  
ENTRY BY: RRR  
CHECKED BY: RDS  
SHEET 2 of 2

**GEOTECHNICAL MEMORANDUM**

Laytonville Dos Rios Road (CR 322) Failure at MP 3.34

CAI File: 16-337.10

April 23, 2018

**APPENDIX B**

**LABORATORY AND FIELD TEST RESULTS SUMMARY**



Job: **Laytonville Dos Rios Road (CR 322) MP 3.34**  
Job No: **16-337.10**  
Date: **3/1/18**

[illegible]



Project Name: Laytonville Dos Rios Road at MP 3.34

CAInc File No: 16-337.10

Date: 2/16/18

Technician: AS

### MOISTURE-DENSITY TESTS - D2216

	1	2	3	4	5
Sample No.	B1-2	B2-1	B2-6	B3-2	B3-3
USCS Symbol	Rock	SC	D. Rock	GP-GC	Rock
Depth (ft.)	10	5.1	30	10.4	15
Sample Length (in.)	5.564	5.669	4.621	5.347	3.989
Diameter (in.)	1.411	1.404	1.411	1.416	1.412
Sample Volume (ft <sup>3</sup> )	0.00503	0.00508	0.00418	0.00487	0.00361
Total Mass Soil+Tube (g)	360.6	391.7	362.1	364.3	362.7
Mass of Tube (g)	138.3	125.1	127.4	134.1	133.5
Tare No.	B11	C13	E5	P91	G14
Tare (g)	13.9	13.7	13.7	131.1	13.6
Wet Soil + Tare (g)	75.6	79.3	71.3	357.8	73.4
Dry Soil + Tare (g)	71.1	75.4	66.8	348.9	68.8
Dry Soil (g)	57.2	61.7	53.1	217.8	55.1
Water (g)	4.5	3.9	4.5	8.9	4.6
Moisture (%)	7.9	6.3	8.4	4.1	8.3
Dry Density (pcf)	90.2	108.8	114.1	100.1	129.1

Notes:



Project Name: Laytonville Dos Rios Road at MP 3.34

CALinc File No: 16-337.10

Date: 2/16/18

Technician: AS/ETT

**200 Wash - ASTM D1140**

Method A

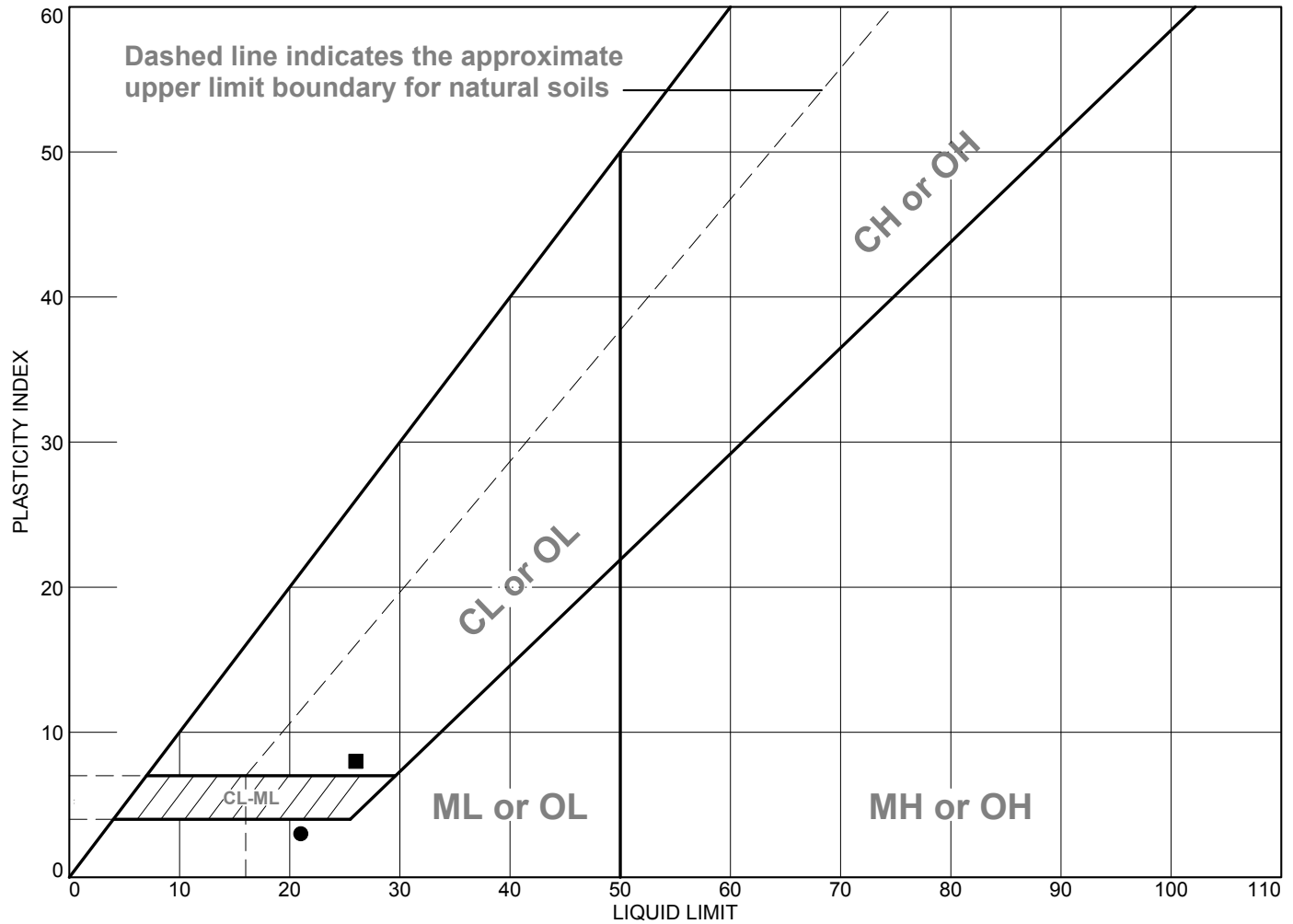
Max Particle Size (100% Passing)	Standard Sieve Size	Recommended Min Mass of Test Specimens
2 mm or less	No. 10	20 g
4.75 mm	No. 4	100 g
9.5 mm	3/8 "	500 g
19.0 mm	3/4 "	2.5 kg
37.5 mm	1 1/2 "	10 kg
75.0 mm	3 "	50 kg

Table from 6.2 of ASTM D1140

Sample No.	Bulk 1	Bulk 2	Bulk 3	B3-2	
USCS Symbol	SC	SC	SC	GP-GC	
Depth (ft.)	0-5	0-5	1-4	10.4	
Tare No.	R19	P20	R15	P91	
Tare (g)	131.1	146.9	130.3	131.1	
Dry Soil + Tare (g)	316.7	422.6	340.5	348.9	
Dry Mass before (g)	185.6	275.7	210.2	217.8	
Dry Mass after (g)	144.9	213.8	137.8	192.8	
Percent Fines (%)	22	22	34	11	

Notes:

# LIQUID AND PLASTIC LIMITS TEST REPORT



	Material Description	Sampled	Tested	Technician	LL	PL	PI	%<#40	USCS
<input type="radio"/>			2/21/18	AST	21	18	3		
<input type="checkbox"/>			2/21/18	AST	26	18	8		

**Project No.** S9763-05- **Client:** Crawford and Associates  
**Project:** Crawford 16-337.10

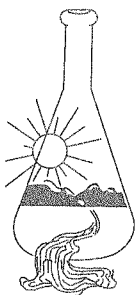
☐ **Location:** Dos Rios Road MP 3.34 **Sample Number:** B2-Bulk  
☐ **Location:** Dos Rios Road MP 3.34 **Sample Number:** B3-Bulk

**GEOCON CONSULTANTS, INC.**

**Checked by:** MR  
**Title:** Lab Manager  
**Figure**

**Tested By:** AST **Checked By:** MR





## Sunland Analytical

11419 Sunrise Gold Circle, #10  
Rancho Cordova, CA 95742  
(916) 852-8557

Date Reported 02/16/2018  
Date Submitted 02/12/2018

To: Ellen Tiedemann  
Crawford & Associates, Inc.  
1100 Corporate Way Suite 230  
Sacramento, CA 95831

From: Gene Oliphant, Ph.D. \ Randy Horney  
General Manager \ Lab Manager

The reported analysis was requested for the following location:  
Location : 16-337.10 - 3.34 Site ID : B2.  
Thank you for your business.

\* For future reference to this analysis please use SUN # 76179-158871.

---

### EVALUATION FOR SOIL CORROSION

Soil pH	6.70		
Minimum Resistivity	0.27	ohm-cm (x1000)	
Chloride	442.2 ppm	00.04422	%
Sulfate	86.7 ppm	00.00867	%

#### METHODS

pH and Min. Resistivity CA DOT Test #643  
Sulfate CA DOT Test #417, Chloride CA DOT Test #422